

ENHANCING STIMULATED EMISSION

Stimulated emission, which is a necessary consequence of interaction of radiation with atoms can be exploited to construct an oscillator or amplifier of radiation at the resonant freq  $\omega_{21}$ .

Consider a collection of atoms exposed to (broad-band) radiation. Let these be 2-level atoms for simplicity. Then the rate at which the energy density, or intensity of the radiation changes is governed by the equations

$$\left. \frac{d\rho}{dt} \right|_{\text{abs}} = -N_1 \hbar \omega_{21} R_{12}$$

$$\left. \frac{d\rho}{dt} \right|_{\text{st.em}} = +N_2 \hbar \omega_{21} R_{21}$$

NOT IMP  $\left. \frac{d\rho}{dt} \right|_{\text{sp.em}} = +N_2 \hbar \omega_{21} R'_{21}$

-  $N_2$ : upper level pop.  $N_1$ : lower level pop.

- of these three, only  $R_{21}$  &  $R_{12}$  depend on  $\rho$ .

$$\begin{aligned} \text{RECAP: } I(\omega) &= c\rho(\omega) = c\hbar\omega(n/V) \\ &= \frac{1}{2} \epsilon_0 E^2(\omega) \end{aligned}$$

$$\sigma_{\text{st.}}(\omega) = \hbar\omega_{21} R_{21} / \hbar\omega$$

The average rate of change of density of the radiation per unit volume of the medium exposed to radiation is

$$\frac{d\rho}{dt} = \sigma I (N_2 - N_1)$$

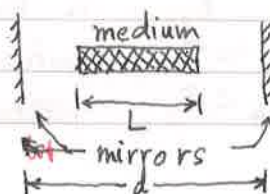
$$\text{or } \left. \frac{dI}{dz} \right| = \frac{d\rho}{dt} = \sigma I (N_2 - N_1) \Rightarrow I = I_0 e^{-\alpha z}$$

where  $\alpha = (N_1 - N_2) \sigma$   
 $[\alpha(\omega)]$   $[\sigma(\omega)]$

If  $N_2 > N_1$ , the density of radiation is enhanced, and if  $N_1 > N_2$  the density is depleted. — we have therefore amplification or attenuation.

If the medium has length  $L$ , then over one return trip of the a radiation pulse, the gain (or loss) will be given as the ratio

$$G = \frac{I(\omega, 2L)}{I(\omega, 0)} = e^{-2\alpha(\omega)L}$$



RECALL Einstein A, B coefficients

Spontaneous emission depopulates  $N_2$  so that thermal equilibrium is maintained. Thus, due to spontaneous emission, we always have

$$N_2/N_1 = \exp(-\hbar\omega_{21}/KT) \quad \text{and} \quad \alpha = N_1 - N_2 \text{ is +ve}$$

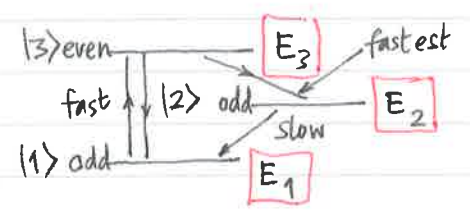
irrespective of the value of  $R_{21}$  [or  $\sigma_{21}$ ]

Thus  $G = \exp[-2\alpha L]$  is always  $< 1$  for a 2-level system. Amplification cannot be achieved by a 2-level system.

A THREE LEVEL SYSTEM

Suppose we have a three-level system which is such that

and  $A_3 > A_2 > A_1$ , i.e.  $\tau_3 < \tau_2 < \tau_1$ , preferably  $\tau_3 \ll \tau_2$   
 and  $R_{23}, R_{13}$  are non-zero  
 and  $R_{12}$  is small



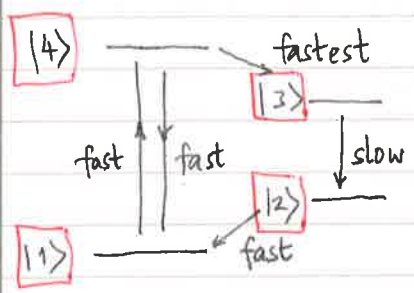
then a "population inversion" may be obtained between levels 2, 1 if  $> 50\%$

of  $N_1$  is transferred to  $N_3$  by stimulated absorption and  $|2\rangle$  is rapidly populated by decay of  $|3\rangle$  rather than  $|3\rangle$  decaying to  $|1\rangle$

- $\Rightarrow R_{32}$  is very high (dipole allowed) while  $R_{21}$  is weak (dipole forbidden)
- $\Rightarrow R_{13}$  or  $R_{31}$  is high (dipole allowed) to ensure population pumping
- $\Rightarrow$  Difficult to meet all conditions simultaneously.

A FOUR LEVEL SYSTEM

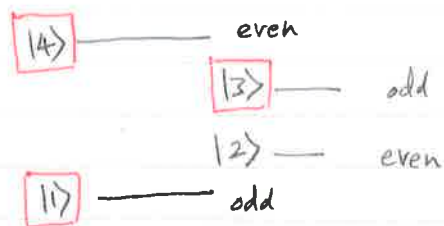
A system such that  $E_1 \rightarrow E_4$  is a fast dipole allowed transition and  $E_3 \rightarrow E_2$  is a slow dipole forbidden transition is a more practical system for achieving population inversion.



- $\Rightarrow R_{43}$  is high
- $R_{21}, R_{12}$  is ~~not~~ high
- $R_{41}, R_{14}$  are high
- $R_{32}$  is low.

$\tau_3 > \tau_2$ , preferably  $\tau_3 \gg \tau_2$   
 $\tau_4 < \tau_3$ , preferably  $\tau_4 \ll \tau_3$

For a four level system to achieve inversion the parities of the 4 levels must be of the type if all transition are radiative.



Ensures  $R_{41}$   $R_{43}$   $R_{21}$  requirements  
But this scheme conflicts with the requirement that  $R_{32}$  should be slow.

⇒ One of the fast transitions  $R_{43}$  or has to be non-radiative.

### THRESHOLD CONDITION FOR LASING

We defined  $\alpha(\omega) = (N_1 - N_2) \sigma(\omega)$  in which 1 and 2 are levels between which lasing occurs.

LASING: enhanced (amplified) emission of radiation at a particular  $\omega$  and  $\hat{E}$  due to stimulated absorption at the same  $\omega$  and  $\hat{E}$ .

SPONTANEOUS & STIMULATED emission rates are equal in a radiation field that contains on an average 1 photon per mode

Ratio of stimulated to spontaneous emission rates gives the number of photons in that mode → we wish to enhance / amplify this.

However, the more the upper level population, the greater is also the absolute value of spontaneous emission rate, thereby reducing the population inversion.

At thermal equilibrium  $N_2 < N_1$ , but if inversion has been achieved by some means  $N_1 < N_2$ , or strictly  $N_1 \frac{g_2}{g_1} < N_2$

If the last condition is satisfied  $\alpha > 0$  (inversion condition)

and  $G(\omega) = \exp(-2\alpha L)$  is positive

There may be

Attenuation / diffraction / reflection losses:  $I(d) / I(0) = e^{-\gamma d}$

where  $d$  is the mirror separation

Then  $G(\omega) = \frac{I(\omega, 2d)}{I(\omega, 0)} = e^{-2\alpha L - \gamma}$

If  $G(\omega) = 1$  we have a stable oscillator, all losses are overcome

Although  $N_2 > N_1$ ,  $N_2/N_1$  is not a constant

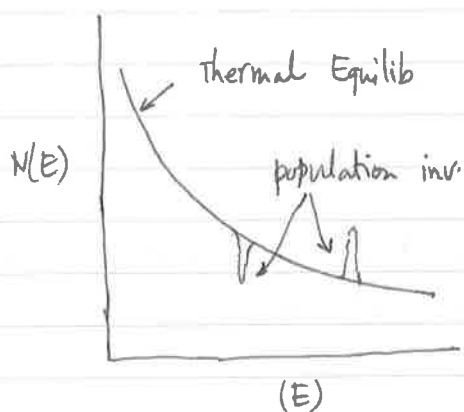
REASON: Increase in photon numbers increases stimulated emission  
stimulated emission reduces population inversion

RESULT:  $N_2/N_1$  settles to an equilibrium condition in a short time

$$\text{For } G(\omega) = 1, \quad 2\alpha L = -\gamma \quad \Rightarrow \quad 2(N_1 - N_2)\sigma_L = -\gamma$$

$$\Rightarrow \Delta N_{\text{thresh}} = \frac{\gamma}{2\sigma_L}$$

$\Delta N > \Delta N_{\text{thresh}}$  makes the oscillator an amplifier



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RECAP:

The rates for spontaneous and stimulated emission are

$$\text{stim: } \begin{cases} R_{21} \\ R_{12} \end{cases} = \frac{\pi e^2}{3 \epsilon_0 \hbar^2} \rho(\omega_{21}) \langle \vec{r}_{21} \rangle^2 \quad \begin{array}{l} [\text{unpolarised } \hat{\mathbf{E}}] \\ [\text{for polarised replace } \vec{r} \text{ by } 3\vec{z} \\ \text{or } 3\hat{\mathbf{E}} \cdot \vec{r}] \end{array}$$

$$\text{spont: } R'_{21} = \frac{4}{3} \frac{e^2}{\pi^2 \hbar^3 c^3 \epsilon_0} \omega_{21}^3 \langle \vec{r}_{12} \rangle^2$$

$$R'_{21} = \frac{e^2}{3\pi \hbar \epsilon_0 c^3} \omega_{21}^3 \langle \vec{r}_{12} \rangle^2$$

The key quantity here is the matrix element  $\langle \vec{r}_{12} \rangle$ . This element has radial and angular integrals:

$$\begin{aligned} \langle \vec{r}_{12} \rangle &= \int \cancel{R_1(r)} \cancel{A_1(\theta, \phi)} \\ &= \int [R_1(r) A_1(\theta, \phi)]^* \vec{r} [R_2(r) A_2(\theta, \phi)] d^3\vec{r} \end{aligned}$$

The radial part of the integral is generally non-zero, but the angular part is non-zero only for certain combinations of the angular momentum quantum numbers.

This condition gives rise to selection rules.

$\hat{\mathbf{E}}$  can be written in spherical components

$$\mathbf{E}_{\pm 1} = \frac{1}{\sqrt{2}} (\mathbf{E}_x \pm i \mathbf{E}_y) \quad \mathbf{E}_0 = \hat{\mathbf{E}}_z$$

If  $\vec{\mathbf{k}} = k_z \hat{\mathbf{z}}$ , then  $\mathbf{E}_{\pm 1}$  are circular polarisation components

$$\text{Then } \hat{\mathbf{E}} \cdot \vec{r} = \sum_{\mathbf{q}} \mathbf{E}_{\mathbf{q}}^* I_{\{\mathbf{1}\}\{\mathbf{2}\}}$$

$$I_{\{\mathbf{1}\}\{\mathbf{2}\}} = \int R_{n_1 l_1}^{(m)} R_{n_2 l_2}^{(r)} Y_{l_1 m_1}(\theta, \phi) Y_{l_2 m_2}(\theta_2, \phi_2) r^3 dr d\Omega$$

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From this we get the following rules for dipole transitions

Parity : must change

magnetic quantum number :

$\Delta m = 0$  for linear pol.  $\hat{E} \parallel \hat{z}$

$\Delta m = \pm 1$  for circular pol.  $\hat{k} \parallel \hat{z}$

orbital angular momentum :

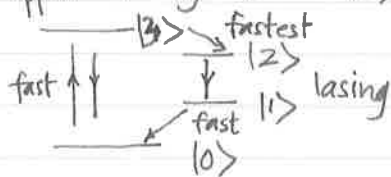
$\Delta l = \pm 1$

total angular momentum

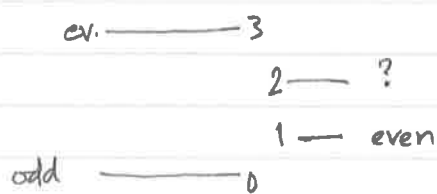
$\Delta j = 0, \pm 1$  but not  $j=0 \rightarrow j=0$

Although a 3-level laser is in principle a workable laser, it puts a serious demand on pumping from  $|1\rangle$  to  $|3\rangle$  to achieve population inversion between  $|2\rangle$  and  $|1\rangle$ , the lasing levels

An alternative is a four level laser, in which the ground state  $|0\rangle$  and the first excited states  $|1\rangle$  are considerably apart ( $\gg kT$ ) and a fast pump is possible from  $|0\rangle$  to  $|3\rangle$ , where  $|3\rangle$  is above the upper lasing level  $|2\rangle$



$|1\rangle$  &  $|0\rangle$  have to be of opp parities,  
 $|3\rangle$  &  $|2\rangle$  also " "



$\tau_3 < \tau_2$  or even better  $\tau_3 \ll \tau_2$   
 $\tau_2 > \tau_1$  or even better  $\tau_2 \gg \tau_1$

Thus  $|2\rangle$  &  $|1\rangle$  have to be of even parity if  $|2\rangle \rightarrow |1\rangle$  is to be weakly forbidden to ensure inversion

If  $|2\rangle$  is even,  $|3\rangle \rightarrow |2\rangle$  can be rapid only if it is non-radiative.

Thus, for a "real" 4-level system, the upper lasing level must be populated non radiatively.

A 4-level laser has the advantage that the lower lasing level is naturally empty, unlike the 3-level system.

## RATE EQUATIONS FOR A 4 LEVEL SYSTEM.

Assume  $|3\rangle$  is pumped from  $|0\rangle$  with some rate  $R$  and that  $|3\rangle$  fills up (pumps into)  $|2\rangle$  at some pump rate 'P'

Assume  $|2\rangle$  radiates to  $|1\rangle$  by with Einstein coeff  $B_{21}$  and has other loss rate  $L_2$  (similarly for  $|1\rangle$ )

Then the rate eqns read

$$\frac{dN_1}{dt} = -N_1 B_{12}(\nu\hbar\omega) + N_2 A_{21} + -N_1 L_1 + N_2 B_{21}(\nu\hbar\omega)$$

$$\frac{dN_2}{dt} = P - N_2 B_{21}(\nu\hbar\omega) - N_2 A_{22} + N_1 B_{12}(\nu\hbar\omega) - N_2 L_2$$

$$\therefore \frac{dN_1}{dt} = \Delta N B_{21}(\nu\hbar\omega) - N_1 L_1 + N_2 A_{22} \quad (1) \quad \left. \begin{array}{l} \{ A_{22} \equiv A \} \\ \{ B_{21} = B_{12} \equiv B \} \\ \{ \Delta N = N_2 - N_1 \} \end{array} \right\}$$

$$\frac{dN_2}{dt} = P - \Delta N B(\nu\hbar\omega) - N_2 L_2 - N_2 A \quad (2)$$

$$\frac{dn}{dt} = -\gamma n + N_2 B_{21}(\nu\hbar\omega) - N_1 B_{12}(\nu\hbar\omega)$$

$$\frac{dn}{dt} = -\gamma n + \Delta N B(\nu\hbar\omega) \quad (3)$$

Under steady conditions each rate is zero

$$\frac{dN_1}{dt} = \frac{dN_2}{dt} = \frac{dn}{dt}$$

Adding first two we get

$$P = N_1 L_1 + N_2 L_2$$

Adding second & third

$$P = \gamma n + N_2 A + N_2 L_2$$

Multiply ① by  $L_2$ , ② by  $L_1$

$$(\Delta N B(\nu\hbar\omega) + N_2 A - N_1 L_1) L_2 = 0$$

$$(P - \Delta N B(\nu\hbar\omega) - N_2 A - N_2 L_2) L_1 = 0$$

$$\Delta N = \frac{(L_1 - A) P}{B\nu\hbar\omega (L_2 + L_1) + A L_1 + L_1 L_2}$$

For inversion  $L_1$  (lower state loss rate)  $>$   $A$  (upper state spontaneous <sup>em</sup> rate)